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Characterization of mercerized cellulose nanofibrils prepared by aqueous counter collision process

Daisuke Tatsumi, Atsushi Kanda and Tetsuo Kondo*

Abstract

Cellulose nanofibrils (CNFs) obtained by aqueous counter collision (ACC) methods have amphiphilic Janus-type properties, which appear markedly for ACC–CNFs prepared from bacterial nanocellulose (BNC) pellicles. The amphiphilic Janus-type surface is exposed because of the mechanism involved in ACC pulverizing of cellulose materials, in which the predominant interactions of the (2 0 0) lattice plane of the cellulose I crystal structure are weak interplanar van der Waals interactions. Such selective cleavage is more likely to occur for highly crystalline BNC. This study focused on alkali-mercerized cellulose samples, which are of lower crystallinity than BNC. The mercerized raw materials were subjected to ACC treatments and their fiber morphologies, crystallinities, and surface properties were compared to those of ACC–CNFs from native samples. In particular, the Wide-angle X-ray diffraction (WAXD) results suggested that the cleavage was most likely to occur at the (1 1 0) plane in nanofibrils derived from cellulose II, unlike (2 0 0) lattice plane for the case of cellulose I. Accordingly, the entire results indicate that the properties of the ACC-treated mercerized CNFs differ greatly from those of conventional ACC–CNFs composed of cellulose I crystalline structure. This is presumably because ACC nanopulverization proceeds depending on the surface structure and crystalline morphology of the raw material.

Keywords: Mercerized cellulose, Aqueous counter collision, Cellulose nanofibril, Cellulose II crystal, Nanopulverization

Introduction

Cellulose nanofibrils (CNFs) are attracting increasing interest for use as building blocks of high-performance materials obtained from renewable sources. They are now widely used as fillers for composite materials [1–8] because of their excellent mechanical properties.

CNFs are generally obtained by mechanical or physicochemical pulverization via fibrillation of natural cellulose pulp fibers to nanometer-scale widths. Three types of processes are typically used to fabricate CNFs [8]. The first two are using mechanical shearing stress with chemical pretreatments, e.g., by TEMPO oxidization [9],

and solely mechanical processes, such as grinding [10]. The third type, i.e., the aqueous counter collision (ACC) method, is a physicochemical process, which involves impingement of two high-speed jets of aqueous suspensions of the raw materials, which are expelled through a pair of opposing nozzles [11–13].

The key aspect of this physicochemical process for the preparation of CNFs is selective interfacial cleavage of weak intermolecular interactions by a propagating elastic–plastic wave generated by the impingement of water jets. The shock waves resulting from ACCs are propagated through the elastic crystalline domains of the initial materials, and thus cleave between the hydrophobic van der Waals (2 0 0) planes normally hidden inside native crystalline cellulose fibers. These hydrophobic planes are eventually exposed on the

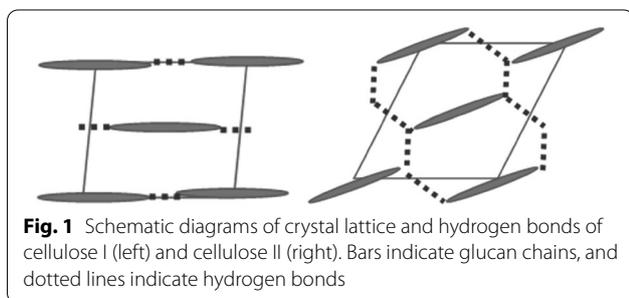
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surface [14]. The resulting CNFs (ACC–CNFs) were found to have a Janus-type amphiphilic surface that is composed of both hydrophobic and hydrophilic planes in an aqueous system [15]. In addition, ACC–CNFs reflect the characteristics of the raw material [16].

Natural cellulose fibers have an internal structure in which the reducing ends of cellulose molecules are aligned in parallel and in one direction. When natural cellulose fibers are subjected to ACC treatment, the ACC–CNFs are expected to be refined from the reducing end during the preparation process. This is confirmed by the observation that thin fibrillated fibers were fibrillated at one end of the thick raw fibers [13, 17].

Mercerization is a process in which natural cellulose fibers are swollen by immersion in highly concentrated aqueous NaOH solution, washed with water, and dried. During this process, the crystal structure is transformed from cellulose I to cellulose II, while retaining its solid phase. Cellulose II crystals consist of anti-parallel arrangements of cellulose molecular chains with alternating reducing ends. In the crystal, hydrogen bonding of the molecular chains occurs not only via O(2)–O(6′) bonds, but also via O(2)–O(2′) and O(6)–O(6′) glucose residue bonds, as shown in Fig. 1. In addition, the crystallinity lower than that of natural cellulose, and is commonly of the order of 60%.

Research to date has only focused on ACC treatment of native cellulose materials. In the ACC treatment of cellulose II, it is still unclear what the surface properties are and which crystal planes are cleaved. The ACC–CNFs from cellulose II are expected to show specific properties that differ from those of conventional ACC–CNFs. In this study, commercially available microcrystalline cellulose (MCC) powder, which had been derived from wood pulp by acid hydrolysis, and its mercerized cellulose were subjected to ACC treatments. The fiber morphologies, crystallinities, and surface properties of the ACC-treated products were investigated. The results are discussed in terms of the cleavage mechanism during the ACC treatment.



It should be noted that because the samples used had similar degrees of crystallinity (ca. 60%), it is preferable to compare the changes in their properties.

Materials and methods

Sample preparation

Commercially available MCC (Funacel II, Funakoshi Co., Ltd., Tokyo Japan) was used as the raw material. The degree of polymerization was 200–220 [13]. The MCC was washed three times with deionized water, twice with a 1:1 (v/v) mixture of deionized water and acetone, and twice with acetone, as described in a previous report [18]. The MCC was used as received (untreated, U). A mercerized (M) sample was obtained by immersion of the MCC in 17.5 wt% NaOH for 30 min, neutralizing, and washing with methanol and ethanol. The two samples were suspended in deionized water at a concentration of 1.0 wt%, and the sample suspensions were subjected to ACC treatment at ejecting pressures of 100 and 200 MPa, and numbers of collisions from 5 to 90 Pass.

The samples were labeled as shown in Table 1; U and M indicate un-mercerized and mercerized, respectively; 100 or 200 is the ejecting pressure and the last numbers are the Pass numbers.

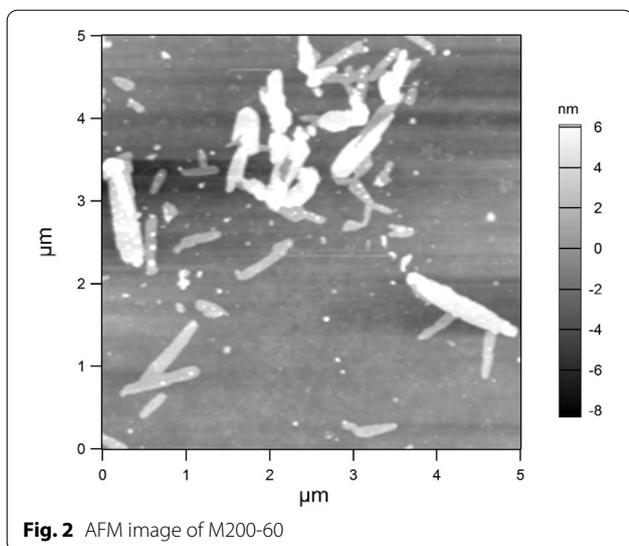
Measurement of fiber lengths and widths

One of the obtained sample dispersions, M200-60, was diluted to 1.0×10^{-4} wt%, cast on a glass substrate, air-dried for more than 1 day, and then examined by atomic force microscopy (AMF). All images were obtained using an MFP-3D Origin instrument (Oxford Instruments Asylum Research, Inc., Santa Barbara, CA, USA), which was operated in AC mode, with a Si-cantilever (OMCL-AC240TS, Olympus Co., Tokyo, Japan), at room temperature. All the obtained images were processed using the accompanying software from Oxford Instruments Asylum Research. ImageJ software was used to determine the fiber lengths from the images.

Small-angle X-ray scattering (SAXS) was performed at the SAGA Light Source BL-11 beamline (Tosu, Saga, Japan), at an energy of 8 keV and a camera length of 2.558 m. The scattering intensities, $I(q)$, of the sample dispersions at 60 and 90 Pass were collected using a PILATUS 300 k detector. The data were circular-averaged using fit2d, for cross-sectional Guinier plotting [19]. The

Table 1 Pretreatments and conditions for ACC processes

Pre-treatment	Ejecting pressure/MPa	Pass number/Pass	Sample name
Untreated (I)	100, 200	5, 10, 30, 60, 90	U100-5 ~ U200-90
Mercerization (II)	100, 200	5, 10, 30, 60, 90	M100-5 ~ M200-90



fiber radius, r ($r = \sqrt{2}R_c$), which corresponds to the fiber width, was calculated from the cross-sectional radius of gyration, R_c , from plots constructed using Eq. (1).

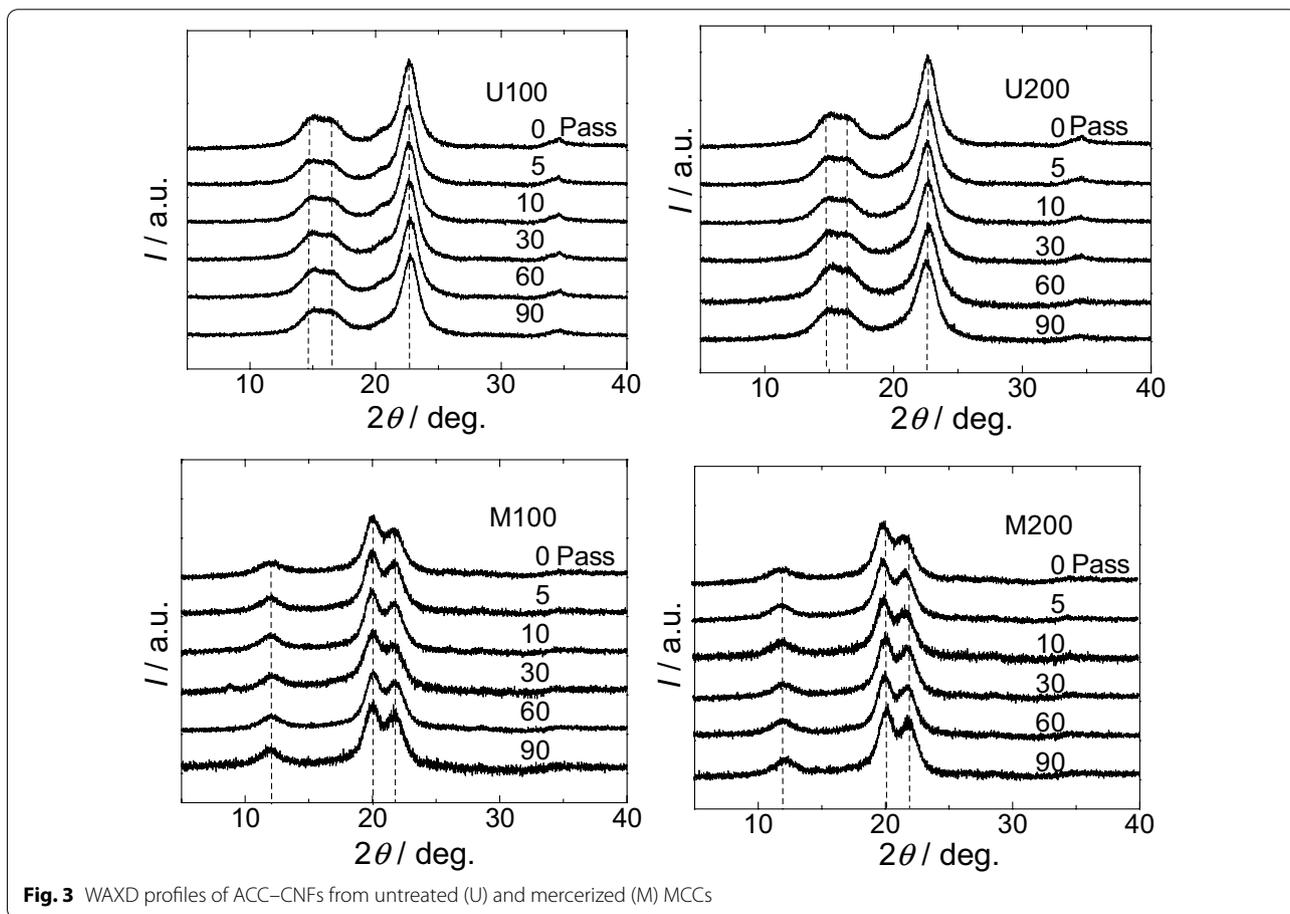
Table 2 Fiber width of samples calculated by cross-sectional Guinier plots

Sample	R_c /nm	Fiber width/nm	Sample	R_c /nm	Fiber width/nm
U100-60	3.55	10.04	M100-60	3.16	8.94
U100-90	3.98	11.26	M100-90	3.16	8.96
U200-60	3.64	10.3	M200-60	3.01	8.50
U200-90	3.49	9.88	M200-90	3.17	8.96

$$\ln I(q)q = \ln I(0)q - \frac{1}{2}R_c^2 q^2 \tag{1}$$

Crystallographic properties

Wide-angle X-ray diffraction (WAXD; SmartLab, Rigaku, Inc., Tokyo, Japan) analysis of freeze-dried samples was performed in the range $2\theta = 5^\circ - 40^\circ$ at a current of 30 mA and a voltage of 40 kV. After removing the amorphous halos, which were caused by the glass substrates, from the obtained diffraction images, the changes in the crystal structures were investigated.



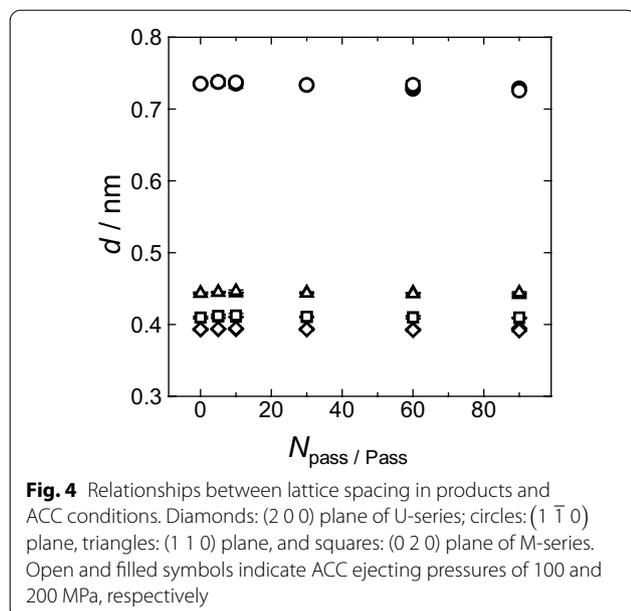


Fig. 4 Relationships between lattice spacing in products and ACC conditions. Diamonds: (2 0 0) plane of U-series; circles: (1 $\bar{1}$ 0) plane, triangles: (1 1 0) plane, and squares: (0 2 0) plane of M-series. Open and filled symbols indicate ACC ejecting pressures of 100 and 200 MPa, respectively

The lattice spacing, d , was determined using Bragg's law:

$$2d\sin\theta = n\lambda \quad (2)$$

where θ is the X-ray incident angle, λ is the wavelength of the incident X-ray, and n represents the reflection order ($n=1$ in this case).

The Scherrer equation was used to calculate the crystal width, w [20]:

$$w = \frac{0.9\lambda}{\beta_{1/2} \cos\theta} \quad (3)$$

where $\beta_{1/2}$ is the half-width of the diffraction line.

The Segal method [21, 22] was used to estimate the crystallinity, CI :

$$CI(\%) = \left(1 - \frac{I_{\text{am}}}{I_{\text{cr}}}\right) \times 100 \quad (4)$$

where I_{am} and I_{cr} are the X-ray diffraction intensities from the amorphous and crystalline regions, respectively. I_{cr} is the intensity from the (2 0 0) plane in cellulose I and from the (0 2 0) plane in cellulose II. For the lattice spacing, crystal width, and crystallinity, the WAXD measurements were repeated three times and the mean values were plotted versus the Pass number.

Surface properties

The fractal dimension, D , of the ACC-treated fibers was calculated from their SAXS profiles. The dependence of the intensity, $I(q)$, on the scattering vector, q , was

introduced into D by extrapolation of the approximate straight lines of the profiles.

Each sample subjected to ACC treatment at 200 MPa and 60 Pass was adsorbed on isotactic polypropylene (iPP; H-500, Prime Polymer Co., Ltd.) and polystyrene (PS; S-20, Sekisui Chemical Industries, Ltd.) particles [16]. The diameter, density, and surface tension of the iPP particles were 500 μm , 0.9 g/cm^3 , and 29 mN/m , respectively [23]. The diameter, density, and surface tension of the PS particles were 300 μm , 1.05 g/cm^3 , and 40 mN/m , respectively [23].

The added amounts of polymer particles and suspension were calculated according to previous reports [16, 24]. The mixed liquid was stirred at 150 rpm for 60 min at room temperature to sufficiently adsorb the nanofibrils on the particles. Excess nanofibrils were removed by washing with deionized water and then the particles were dried at 50 $^{\circ}\text{C}$ for 1 day or more. The polymer particles were stained with calcofluor white (CFW), which is a fluorescent probe specific for cellulose. Excess CFW was removed by washing with deionized water, and the particles were dried by the procedure used for drying the unstained particles. The adsorption of the fibers on each type of polymer particle was examined by confocal laser scanning microscopy (CLSM; TCS SP8 STED, Leica Inc., Wetzlar, Germany) at 410–470 nm, with an excitation wavelength of 405 nm [15, 16].

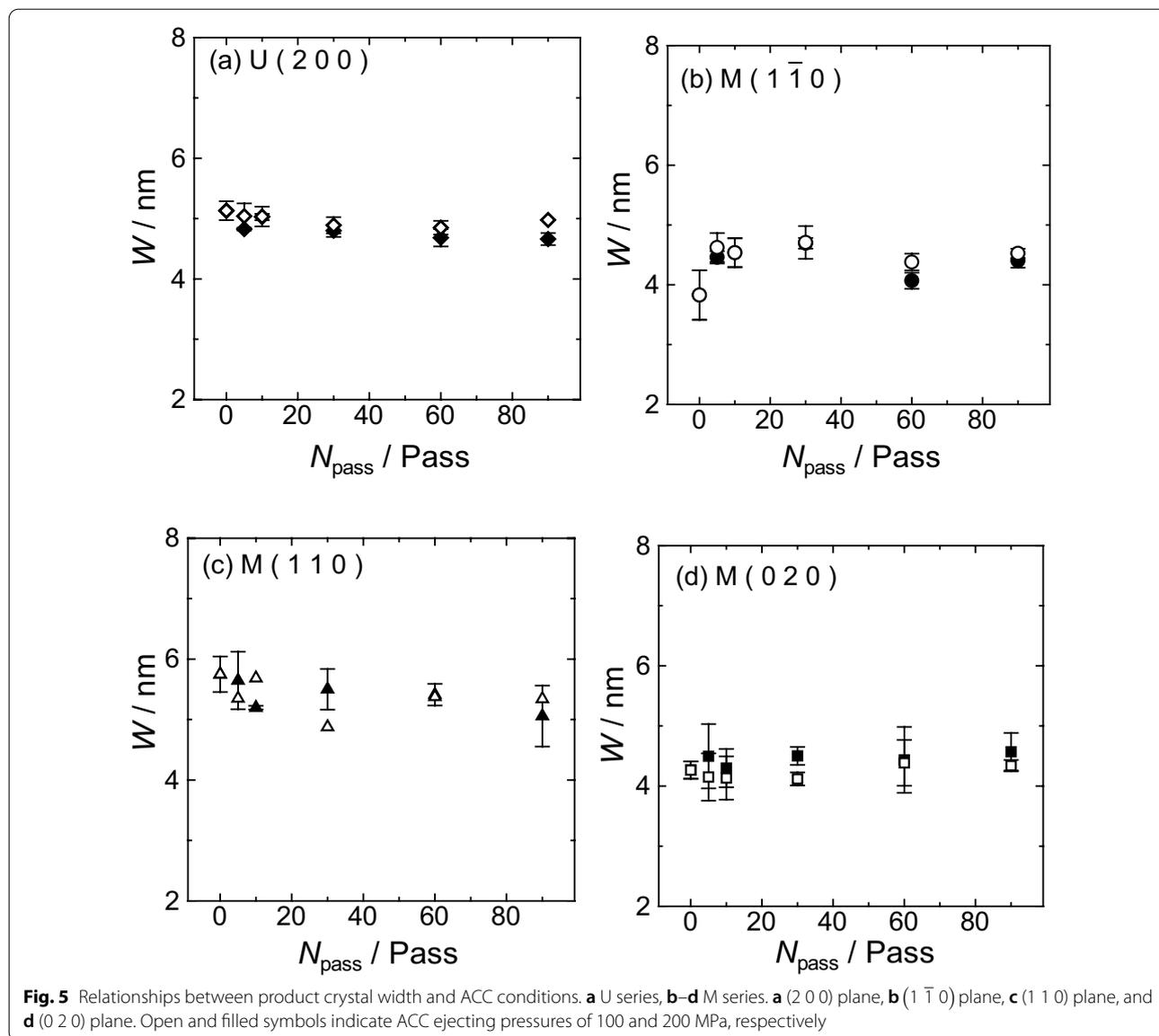
Results and discussion

Fiber length and width

An AFM image of M200-60 is shown in Fig. 2. The fibers of the ACC-treated mercerized MCCs were shorter than those of ACC-CNFs derived from BNC [15]. Image J software was used to estimate the mean fiber length, which was 773.7 ± 343.8 nm ($n=65$), and the mean fiber width (as height), which was 5.57 ± 2.06 nm ($n=50$). AFM enabled determination of the fiber lengths and widths under dry conditions. Cross-sectional plots obtained from SAXS profiles were used to determine the widths of the fibers in suspension. The data are shown in Table 2. The data obtained using AFM and SAXS show that the widths of cellulose II-derived fibers tend to be smaller than those of cellulose I-derived ones. These results indicate that the degree of pulverization may differ depending on the crystal structure of the raw material, i.e., cellulose I or II.

Crystallographic properties

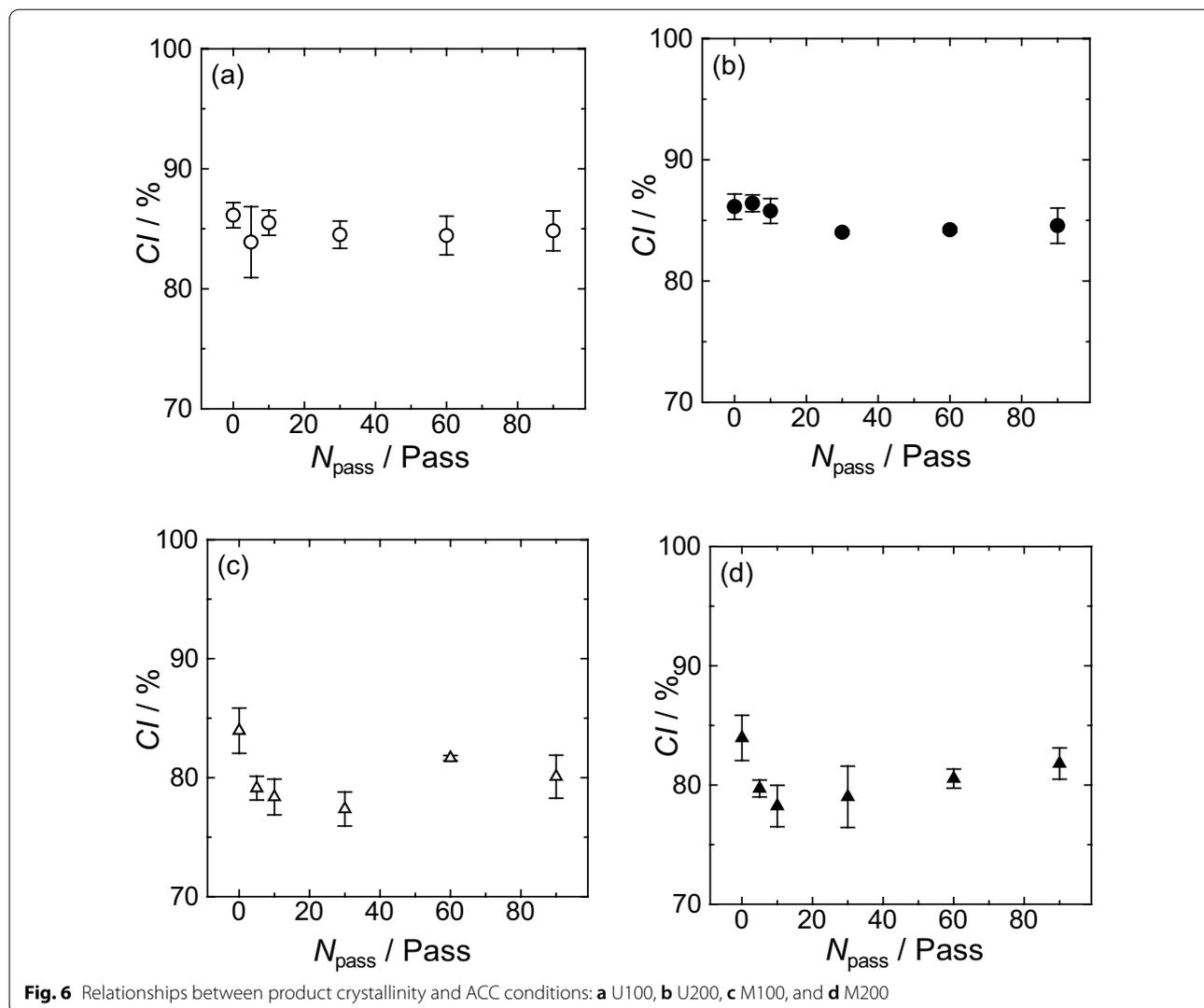
The WAXD profiles of the samples confirmed that the U-series samples had the crystal structure of cellulose I, whereas the M-series samples had the crystal structure of cellulose II. This shows that both series of samples



retained the original crystal structure after ACC treatment (Fig. 3), although different collision pressures and Pass numbers were used. The diffraction peak from the (2 0 0) plane is the most intense for cellulose I, at which the ACC cleavage is considered to occur. The individual lattice spacings for the (1 $\bar{1}$ 0), (1 1 0), and (0 2 0) planes of cellulose II were calculated using Eq. (2). The relationship between the lattice spacings and ACC conditions is shown in Fig. 4; the open symbols (ACC at 100 MPa) and the filled symbols (ACC at 200 MPa) are nearly superimposed. Each plot shows that the lattice spacings are almost constant, i.e., they are independent of the Pass number. A previous study showed that the lattice spacing and crystal width are almost constant, regardless of

the number of collisions, for cellulose I under an ejecting pressure of 200 MPa [13]. These results show that ACC treatment does not change the lattice spacings of mercerized cellulose I, as well as cellulose I samples, under the ejecting pressures and Pass numbers used.

The Scherrer equation was used to calculate the crystal widths for the (2 0 0) plane of the U-series samples, and those for the (1 $\bar{1}$ 0), (1 1 0), and (0 2 0) planes for the M-series samples. The widths before and after ACC treatment were compared, as shown in Fig. 5. The crystal width along the (2 0 0) plane of the U-series samples decreased with increasing Pass number. In contrast, the crystal widths along the (1 $\bar{1}$ 0) and (0 2 0) planes of the M-series samples did not depend on the Pass number. However, the



crystal width along the (1 1 0) plane tended to decrease with increasing Pass number. The decrease in the crystal width along the (2 0 0) plane of the U-series sample indicates that cleavage during ACC treatment probably occurs at this plane. In contrast, the crystal width along the (1 1 0) plane tended to decrease with increasing Pass number for the M-series samples. The value obtained by dividing W by each d -spacing (W/d) indicates how many layers of crystal width decreased in d -spacing units. The value exhibited that the widths for U- and M-series samples decreased by about 10 layers along the (2 0 0) and (1 1 0) planes, respectively. It is, therefore, assumed that cleavage during ACC treatment begins at the (1 1 0) plane in mercerized cellulose. However, a more detailed

investigation is needed. The changes in the crystallinity of each sample are shown in Fig. 6. According to a previous report [13], when cellulose I fibers were subjected to ACC treatment at 200 MPa, the crystallinity initially decreased with increasing Pass number and then increased. In the current study, similar behavior was observed during ACC treatment of cellulose II.

Surface properties

Figure 7 shows double-logarithmic plots of the SAXS peak intensities versus the scattering vector, q . The relationship in the q range from -1 to 0 is linear for U100 and convex upward for U200. For both M-100 and

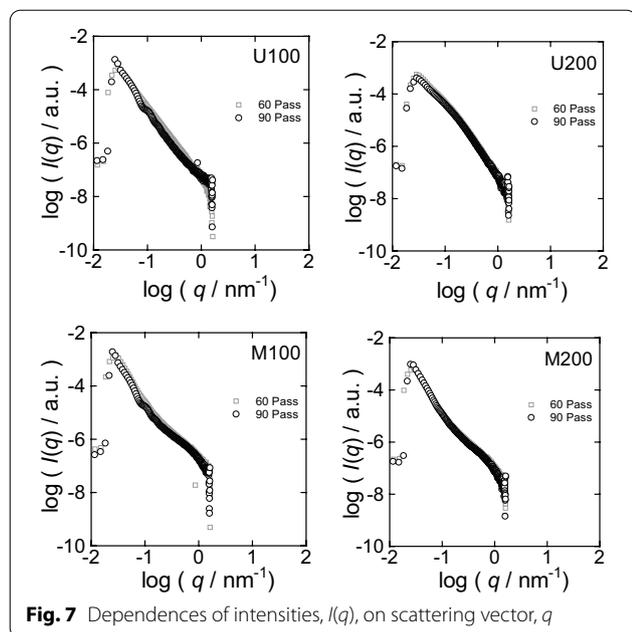


Fig. 7 Dependences of intensities, $I(q)$, on scattering vector, q

Table 3 Fractal dimensions, D , obtained from SAXS profiles

Sample	D	Sample	D
U100-60	2.69	M100-60	1.77
U100-90	2.40	M100-90	1.60
U100-60	2.96	M100-60	1.82
U100-90	2.95	M100-90	1.83

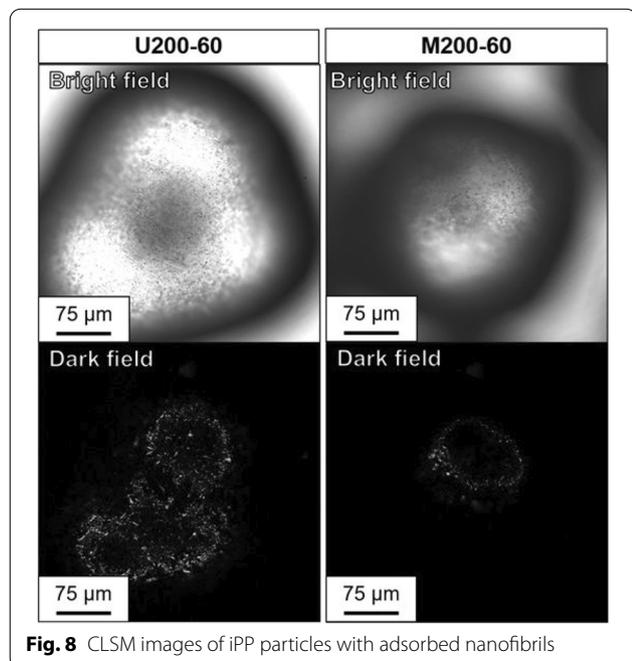


Fig. 8 CLSM images of iPP particles with adsorbed nanofibrils

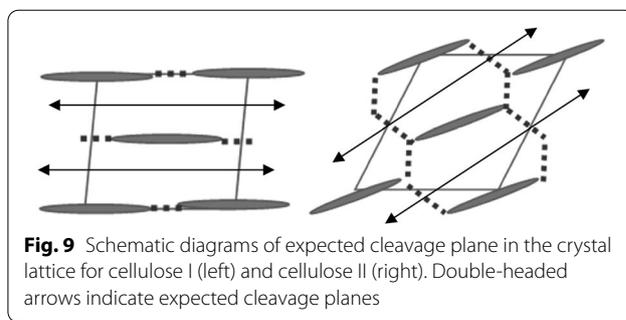


Fig. 9 Schematic diagrams of expected cleavage plane in the crystal lattice for cellulose I (left) and cellulose II (right). Double-headed arrows indicate expected cleavage planes

M-200, the relationship is convex downward. The fractal dimension, D , which was calculated from the approximate straight lines in the U-series plots, is close to 2.5 for U100 and 3 for U200. This shows that D increases with increasing degree of nano-pulverization. In contrast, no differences between the D values for cellulose II were observed at the different ejection pressures, i.e., both are below 2 (Table 3). The fractal dimensions, D , obtained from the SAXS profiles reflect the presence of structures with dimensions of the order of several to 100 nm in the samples [25]. It should be noted that a structure is two-dimensional if D is close to 2, but three-dimensional if it is close to 3. The surfaces of the M-series samples are, therefore, assumed to be more planar than those of the U-series samples. It has been reported that ACC-CNFs are formed by progressive nano-pulverization during fibrillation [13]. It is possible that the increase in the fractal dimension caused by the ACC ejection pressure as nano-refinement progresses reflects formation of finer nanofibrils on the surface. Before ACC treatment, the mercerized cellulose starting material has a smooth surface and a uniform internal structure [26]. It is expected that a planar fractal dimension will be observed after ACC treatment. This implies that during pulverization mercerized cellulose maintains its homogeneous internal architecture under the same ACC-treatment conditions as those used for formation of native ACC-CNFs.

Finally, the surface properties of the ACC products were investigated by examining their adsorption on polymer particles [15, 16]. Figure 8 shows CLSM images of polymer particles coated with the produced ACC-CNFs. Fluorescence attributed to CFW on the CNFs is observed in the iPP particle images. CFW stains cellulose; therefore, these images indicate that nanofibrils of cellulose I and cellulose II are both adsorbed on the iPP particle surfaces. However, the amount of cellulose II adsorbed was less than that of cellulose I. In addition, neither type of nanofibril was adsorbed on PS particles. The results suggest that the capacity for ACC-mercerized

CNF adsorption on the iPP particle surfaces was lower than that for cellulose I-derived ACC–CNFs. This indicates that the differences among the surface properties of the fiber samples can be attributed to differences in the surfaces exposed by ACC cleavage. The adsorption of ACC–CNFs from cellulose I on iPP particles is, therefore, verified to be the result of exposure of the van der Waals surface, i.e., the (2 0 0) plane, by the ACC treatment [16].

The WAXD results suggest that cleavage occurred at the (1 1 0) plane in nanofibrils derived from cellulose II. Yamane et al. used molecular mechanics simulations to investigate the surface properties of cellulose II. They reported that the (1 $\bar{1}$ 0) plane is hydrophilic, and the (1 1 0) plane is more hydrophobic, in cellulose II [27]. During ACC treatment of cellulose II, the hydrophobic (1 1 0) plane is probably exposed, as in the case of cellulose I. However, in the case of cellulose II, hydrogen bonds are also present between molecular chain sheets; therefore, this plane is probably less hydrophobic than the (2 0 0) plane of cellulose I.

Conclusion

The behavior of mercerized CNFs obtained by ACC treatment of mercerized cellulose indicates that the surface structure of the mercerized CNFs depends on the crystal structure of the raw material, similarly to the case for conventional native CNFs. The crystal structure of mercerized cellulose differs from that of native cellulose; therefore, it is indicated that the lattice plane at which cleavage begins during ACC treatment also differs. The most probable cleavage plane in cellulose II is the (1 1 0) plane as shown in Fig. 9. This will be clarified in the future using methods, such as double staining [15].

These findings suggest that a surface with various characteristics can be exposed on the CNFs by changing the crystal structures of the original cellulose and subjecting the original material to ACC treatment. This will enable the development of non-chemical surface-modification methods.

Abbreviations

ACC: Aqueous counter collision; AFM: Atomic force microscopy; BNC: Bacterial nanocellulose; CFW: Calcofluor white; CI: Crystallinity index; CLSM: Confocal laser scanning microscopy; CNFs: Cellulose nanofibrils; iPP: Isotactic polypropylene; MCC: Microcrystalline cellulose; PS: Polystyrene; SAXS: Small-angle X-ray scattering; WAXD: Wide-angle X-ray diffraction.

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Authors' contributions

DT: Research plan and mainly responsible for preparation of the paper. AK: Mainly responsible for performing all experiments. TK: Research plan through study and preparation of the paper.

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Not applicable.

Declarations

Competing interests

The authors declare that they have no competing interests.

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